



Numerical investigation of the seismic response of classical multi-drum and monolithic columns

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Structural characteristics of classical Greek temples

- Greek classical temples constitute world class monuments of great historical, architectural and cultural value.
- Most of them are built from 6th century BC to 3rd century AC
- Few of them remain entirely intact. The majority remain nowadays as free-standing multi-drum or monolithic columns and portals



Parthenon, Acropolis Athens (5th BC)



Temple of Athena Lindia, Acropolis of Lindos, Rhodes (6th BC)



Structural characteristics

- The technology applied for their construction is very advanced
- Each column is composed of several drums often of high-quality marble, which are placed one on top of the other, without connecting mortar. It is a genius mechanical system having high capacity to efficiently absorb seismic motion
- Polos (pin) and empolio (plug)









Seismic response

- The response to seismic ground shaking of multi-drum columns is quite distinct compared to that of modern structures
- A free standing multi drum column has **no eigenvalues**!
- Rocking and/or sliding of the drums along their interfaces control the response, with significant energy dissipation during shaking
- Monolithic columns vs multi-drum columns

Controlling parameters

- ✓ Slenderness
- ✓ Frequency of ground excitation
- ✓ Amplitude of ground excitation
- ✓ Epistyle (i.e., connecting beam)
- ✓ Friction coefficient among drums





Validation of the numerical modelling Numerical versus experimental results



Shaking table model of multi-drum column





NTUA

Deformation patterns

Uniaxial loading with:

- Ricker wavelet with PGA = 0.60 g and frequency f_o = 3.30 Hz (1.8 Hz in prototype scale)
- Ricker wavelet with PGA = 0.80 g and frequency f_o = 2.20 Hz (1.2 Hz in prototype scale)
- Ricker wavelet with PGA = 1.0 g and frequency f_o = 2.75 Hz (1.4 Hz in prototype scale)





Collapse of the column for rather long period Ricker pulses

Validation of numerical modelling

Experimental results vs Numerical Modelling

Input motions:

2 Ricker wavelets 0.6g, f_0 =3.3Hz 1.0g, f_0 =2.75Hz

1 real record: Lefkada 2003 EQ, 0.41g





Investigating friction coefficient on the seismic response of Greek temple columns and multi-drum versus monolithic free-standing column



Acropolis of Lindos, island of Rhodes, Greece





Numerical analysis



Three-dimensional full dynamic time history analyses in ABAQUS



Effect of the friction coefficient



Loma Prieta excitation, uniaxial (x) loading, scaled to PGA = 0.52 g



Effect of the friction coefficient μ = 0.7, PGA=0.6g







Step: Dynamic Frame: 199 Total Time: 2.000000

Erzincan excitation scaled to PGA = 0.6g and friction coefficient of μ = 0.7



Effect of the friction coefficient μ =0.1, PGA=0.6g



Erzincan excitation scaled to PGA = 0.6g and friction coefficient of μ = 0.1



Multi-drum versus monolithic free-standing column

Deformedshapesatthecompletion of the analysisTimewindowsofthenormalstresses σ and shear stresses τ ondiametricallyopposedpointsAand B of the base of the columnduring shaking

- Top: Loma Prieta, uniaxial (x) loading, PGA = 0.52 g
- Bottom: Erzincan, biaxial (x+y) loading, PGA = 0.40 g (long period seismic motion)





Multi-drum versus monolithic free-standing column

Absolute displacement time histories

Uniaxial loading Loma Prieta record scaled to PGA = 0.52g friction coefficient $\mu = 0.7$







Multi-drum versus monolithic free-standing column

Effect of the friction coefficient

Contours of the dynamic part of the normal stresses σ computed at the base of the column (base drum–stylobate interface) during uniaxial (x) shaking.

Loma Prieta record (PGA = 0.52 g)





Structural performance of the multi-drum column





Fundamental remarks

- Monolithic columns are more vulnerable than multi-drum ones
- The **friction coefficient** and its dynamic evolution along the drum interfaces during the dynamic excitation is a **very important factor** controlling the seismic response
- The monolithic column exhibited a higher rocking and rolling response along its base compared to the multi-drum one. The difference was generally higher for high-frequency seismic excitations
- The PGA of the base excitation was found to be a very poor intensity measure for this type of structures
- The SD_{max} of the base excitation was found to better describe the performance and stability of the multi-drum column (generally stable for SD_{max} < D/2, where D the diameter of the base drum)



Publications

- Pitilakis K, Tsinidis G, Karafagka S (2017). Analysis of the seismic behavior of classical multi-drum and monolithic columns. Bulletin of Earthquake Engineering, 15(12):5281–5307, https://doi.org/10.1007/s10518-017-0160-4.
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- Pitilakis K, Karafagka S, Karatzetzou A, Riga E, Manakou M (2022). How safe is Acropolis of Athens and its monuments to low probability earthquakes? Lancellotta, Viggiani, Flora, de Silva & Mele (Eds), Geotechnical Engineering for the Preservation of Monuments and Historic Sites III, Proceedings of the Third international symposium on Geotechnical Engineering for the preservation of monuments and historic sites (TC301-IS 2022), 22-24 June, Napoli, Italy, DOI 10.1201/9781003308867-53.



Thank you



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